

## Supporting Information

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### S1. Determination of the liquidus (LC) and solidus compositions (SC)

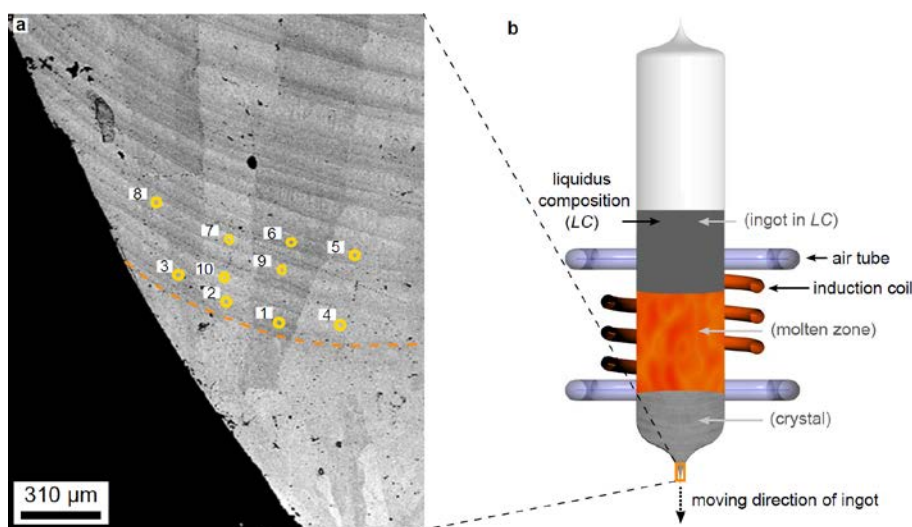


Fig. S1. Determination of liquidus compositions (LC) and their corresponding solidus compositions (SC). (A) Electron probe microanalysis (EPMA) on the LC of Bi : Sb : Te = 10.45 : 28.38 : 61.17 in at. % (see Table S1, sample “3.57E19” and “3.29E19”). Yellow circles and numbers indicate locations of composition measurements and the order of the measurements, respectively. Orange dotted line shows where texturing of the zone-melted crystal begins. This part of the crystal is from the tip of the zone-melted crystal as schematically represented in a cross-sectional view of the ingot being zone-melted (B).

The liquidus compositions (LC) and their corresponding solidus compositions (SC) were determined by an iterative process. For example, as a candidate for LC, an ingot with a composition of Bi : Sb : Te = 10.45 : 28.38 : 61.17 (in at. %) was zone-melted as in Fig. S1B. Unlike in Fig. 2A (main text), only one ingot (of LC) is used which results in the zone-melted crystal with a concentration gradient along the height of the crystal. Therefore, in order to accurately measure the freezing composition of the melted LC, electron probe microanalysis (EPMA) was done on the region where the molten zone was first solidified (orange square in Fig. S1B). The orange dotted line in Fig. S1A clearly defines the boundary between the textured crystal (curved layers) and the crystal without homogeneous orientation (below the line). Since the start of the textured crystal corresponds to that of the molten zone, EPMA measurements from ten different spots (yellow circles in Fig. S1A) were taken from above the orange dotted line (but still close to the line). Those spots were deliberately chosen to be closer to the surface of the crystal as the cooling air (via air tube in Fig. S1B) first froze the melted ingot near the surface. According to the EPMA, the averaged (from ten data points) content ratio of Sb to Bi was  $0.76 (\pm 0.06)$  (when Bi content was set to 0.25 for clarity) and the averaged Te was 60.55 at. %. As the freezing composition had an excess Te content ( $> 60.0$  at. %) while keeping the content ratio of Bi to Sb as 0.25 : 0.75 (expressed as  $(\text{Bi}_{0.25}\text{Sb}_{0.75})_2\text{Te}_{3+6}$ ) the composition of Bi : Sb : Te = 10.45 : 28.38 : 61.17 (in at. %) and its freezing composition were adopted as LC and SC, respectively. This combination of LC and SC was used in the samples “3.57E19” and “3.29E19” as listed in Table 1 (main text) and Table S1 below. After the sample “3.29E19” was synthesized, the same synthesis procedure was repeated to make “3.57E19” from the very beginning for a brief reproducibility test. All the LC used in Table 1 of main text, their freezing compositions estimated by EPMA

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are given in Table S1. For SC of the sample “4.57E19”, lower limit of the estimated Te (at. %) from the freezing composition was used.

Table S1 Freezing composition of each LC measured by EPMA.

Sample <sup>†</sup>	LC			freezing composition <sup>‡</sup>		SC		
	Bi (at. %)	Sb (at. %)	Te (at. %)	Bi : Sb	Te (at. %)	Bi (at. %)	Sb (at. %)	Te (at. %)
4.57E19	10.30	28.10	61.60	0.25 : 0.74 ( $\pm 0.05$ )	60.30 ( $\pm 0.17$ )	9.97	29.90	60.13
3.61E19	10.30	28.10	61.60	0.25 : 0.74 ( $\pm 0.05$ )	60.30 ( $\pm 0.17$ )	9.92	29.78	60.30
3.57E19	10.45	28.38	61.17	0.25 : 0.76 ( $\pm 0.06$ )	60.55 ( $\pm 0.14$ )	9.862	29.58	60.55
3.29E19								
2.64E19	10.46	27.92	61.61	0.25 : 0.79 ( $\pm 0.03$ )	61.16 ( $\pm 0.54$ )	9.71	29.12	61.17

<sup>†</sup> Sample name =  $n_H$  of the resulting zone-levelled crystal at 300 K

<sup>‡</sup> freezing composition = composition that melted LC ingots freeze into

## S2. Thermoelectric transport properties

The transport properties of the zone-levelled samples of  $(\text{Bi}_{0.25}\text{Sb}_{0.75})_2\text{Te}_{3+\delta}$  at 300 K including Hall carrier concentration and Hall mobility ( $\mu_H$ ) are given in Table S2. Each sample was named with its Hall carrier concentration value ( $n_H$ ) at 300 K (Table 1 in main text).

Table S2 Transport properties of zone-levelled  $(\text{Bi}_{0.25}\text{Sb}_{0.75})_2\text{Te}_{3+\delta}$  at 300 K.

Sample <sup>†</sup>	$n_H$ ( $\text{cm}^{-3}$ )	$S$ ( $\mu\text{V/K}$ )	$\sigma$ (S/cm)	$\mu_H$ ( $\text{cm}^2/\text{Vs}$ )	$\kappa$ (W/mK)	$zT$
6.73E19	6.73E19	142.6	2334	216.3	2.20	0.65
4.57E19	4.57E19	180.8	1515	207.0	1.89	0.79
3.61E19	3.61E19	158.8	1667	288.4	1.90	0.66
3.57E19	3.57E19	162.4	2280	399.0	1.96	0.92
3.29E19	3.29E19	156.8	2450	464.9	1.88	0.96
2.64E19	2.64E19	180.6	1885	444.9	1.76	1.05

<sup>†</sup> Sample name =  $n_H$  of the resulting zone-levelled crystal at 300 K.

## S3. Two-band transport model

A two-band (TB) model was employed to compute transport properties of the zone-levelled  $(\text{Bi}_{0.25}\text{Sb}_{0.75})_2\text{Te}_{3+\delta}$  samples at 300 K. For each nonparabolic band, Boltzmann transport equations (as functions of chemical potential) were numerically solved (in Python) to obtain chemical potential dependent thermoelectric parameters (i.e. Seebeck coefficient, carrier concentration, mobility, Hall coefficient, and Lorenz number.) while assuming acoustic phonon scattering[1] and alloy scattering[2] (no alloy scattering for  $\text{Bi}_2\text{Te}_3$  and  $\text{Sb}_2\text{Te}_3$ ). The resulting transport properties from the two valence bands ( $VB_1$  and  $VB_2$  in Fig. 1 of main text) were calculated by taking conductivity-weighted averages of the thermoelectric parameters of each band[3].

The energy gap between the lowest conduction band (CB) and the highest valence band for  $0 \leq x \leq 0.75$  ( $VB_1$ ) used in the TB model was taken from Sehr *et al.*[4] (Fig. 1 of main text and  $\Delta E_{CB-VB1}$  in Fig. S3A). For  $x > 0.75$ , the  $\Delta E_{CB-VB1}$  (green in Fig. S3A) was linearly extrapolated to minimize complexity. In order to determine the energy gap ( $\Delta E_{CB-VB2}$ ) between the CB and the second highest valence band ( $VB_2$ ), the density-of-states effective mass ( $m^*$ ) and deformation potential ( $E_{def}$ ) for each valence band at  $x = 0$  and  $x = 1$  were first tentatively fitted to experimental data from the literature while adjusting  $\Delta E_{CB-VB2}$  (purple in Fig. S3A) at  $x = 0$  and 1. We chose to start the fitting from  $x = 0$  ( $\text{Bi}_2\text{Te}_3$ ) and  $x = 1$  ( $\text{Sb}_2\text{Te}_3$ ) because we did not have to consider the alloy scattering at these compositions and there were many experimental literature data points available for more accurate fitting (as in Figs. S4A, S4B, S6C, and S6d). Our analysis is consistent with the two valence bands are crossing at  $x = 0.75$ :  $\Delta E_{CB-VB2}$  at  $x = 0.75$  is the same as the  $\Delta E_{CB-VB1}$  at  $x = 0.75$  (from Sehr *et al.*[4]). It was found that the  $\Delta E_{CB-VB2}$  at  $x = 0.75$  and the fitted  $\Delta E_{CB-VB2}$  at  $x = 0$  and 1 could be joined in a straight (with small deviations). For simplicity, the  $\Delta E_{CB-VB2}$  was assumed to change linearly with the composition ( $x$ ), and the

$\Delta E_{CB-VB2}$  for other  $x$  were obtained from the straight line joining the  $\Delta E_{CB-VB2}$  at  $x = 0.75$  and that at  $x = 0$  (for  $x = 1$ , their  $m^*$  and  $E_{def}$  were refitted with the updated  $\Delta E_{CB-VB2}$  at  $x = 1$ , which was then on top of the line joining the  $\Delta E_{CB-VB2}$  at  $x = 0.75$  and 0). For  $0.75 < x \leq 1$ , the highest valence band is the  $VB_2$  and the  $\Delta E_{CB-VB2}$  serves as the energy gap (between the lowest  $CB$  and the highest valence band). The fitted energy gap at  $x = 1$  used in the TB model (0.2007 eV of  $\Delta E_{CB-VB2}$  in Fig. 3SA) is about 16 % smaller than degeneracy-corrected optical energy gap from Sehr *et al.*[4] (reasonable given the tendency to overestimate the optical energy gap as degeneracy increases)[5].

Based on the band structure information ( $\Delta E_{CB-VB1}$  and  $\Delta E_{CB-VB2}$  shown in Fig. 3SA) obtained from the literature and the fitting to the experimental literature data of  $x = 0$  and 1, the  $m^*$  and  $E_{def}$  of each band for  $0 < x < 1$  were also fitted to the experimental literature data (for  $x = 0.75$ , the zone-levelled  $(Bi_{0.25}Sb_{0.75})_2Te_{3+\delta}$  samples were also included). As shown in Figs. 3SB and 3SC, both the  $m^*$  and  $E_{def}$  varied linearly with the composition  $x$ . For  $Bi_2Te_3$ - $Sb_2Te_3$  alloys ( $0 < x < 1$ ), a reduction of carrier mobility due to electron scattering from atomic disorder (the same disorder that decreases the lattice thermal conductivity from point defect scattering) was taken into account in the TB model. As the mobility is related to the total relaxation time, the total relaxation time used for  $0 < x < 1$  was calculated by Matthiessen's rule:  $\tau_{total}^{-1} = \tau_{ac}^{-1} + \tau_{alloy}^{-1}$ , where  $\tau_{ac}$  and  $\tau_{alloy}$  were the relaxation times for acoustic phonon scattering and alloy scattering, respectively. In the  $\tau_{alloy}$  equation (from Wang *et al.*[2]) used in the TB model, there was a free parameter  $U$  that determined the magnitude of the electron scattering from alloy disorder. A constant  $U$  of 0.35 eV was used for all  $x$ .

Anisotropy of the bands was also considered in the TB model. Stordeur *et al.*[6] have optically measured effective masses along longitudinal ( $m_{||}^*$ ) and transverse ( $m_{\perp}^*$ ) ellipsoid directions. However, since Stordeur *et al.* assumed that only a single band was participating in transport only composition-dependent  $m_{||}^*$  and  $m_{\perp}^*$  for a single valence band was available. Hence, in the TB model the  $m_{||}^*/m_{\perp}^* = 2.29$  (Stordeur *et al.* reported this value for  $x = 0.75$ ) was assumed for both valence bands and for all  $x$  to minimize the complexity.

The elastic constants ( $C_l = d \times v_l^2$  where  $d$  and  $v_l$  are the density and the longitudinal sound velocity, respectively) of  $Bi_2Te_3$  ( $x = 0$ ) and  $Sb_2Te_3$  ( $x = 1$ ) were calculated from the  $d$  and  $v_l$  of  $x = 0$  ( $d = 7700 \text{ kg/m}^3$  and  $v_l = 2143 \text{ m/s}$  from ref. [7, 8]) and  $x = 1$  ( $d = 6500 \text{ kg/m}^3$  and  $v_l = 2333 \text{ m/s}$  from ref. [7, 8]). The  $C_l$  for the rest  $x$  were linearly interpolated between those of  $x = 0$  and 1 (Fig. S3D).

As shown in Figs. S4, S5, and S6, band parameters used in the TB model (Fig. S3) yielded satisfactory fits to the experimental literature data at 300 K. The underlying physics of the measured transport properties in  $(Bi_{1-x}Sb_x)_2Te_3$  single/oriented crystals is satisfactorily captured in the fits provided by the TB model. The linearly changing band parameters (with respect to the composition  $x$ ) determined from the TB model and the satisfactory fit of the TB model to the experimental data strongly confirm that the band convergence at  $x = 0.75$ .

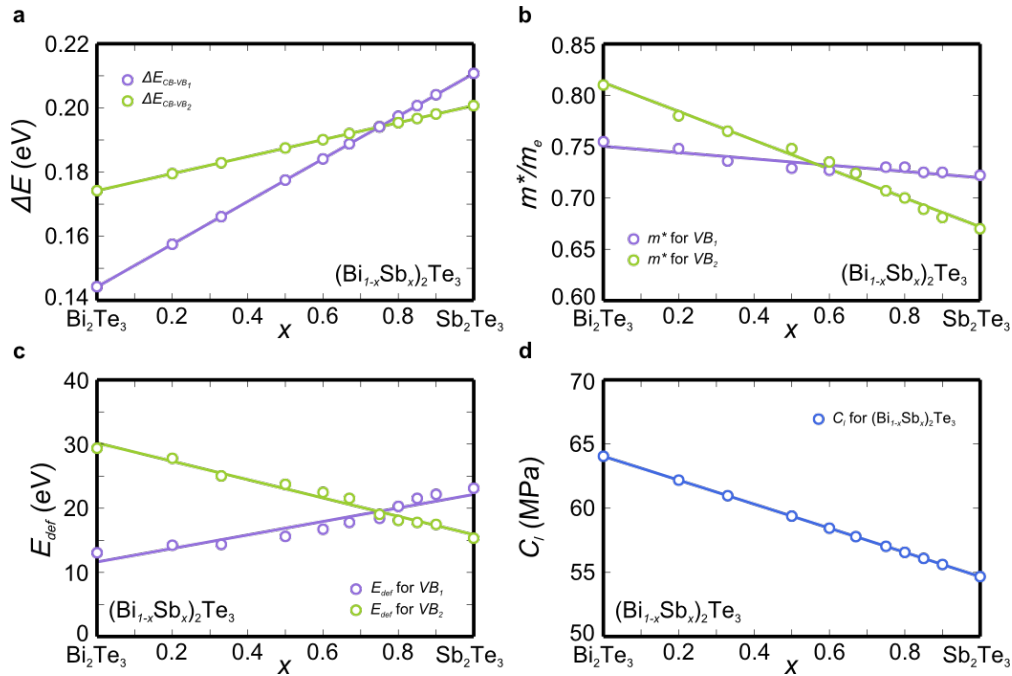


Fig. S3. Composition-dependent band parameters used in the TB model. The energy gap ( $\Delta E$ ) between the lowest conduction band and each valence band (A), the density-of-states effective mass ( $m^*$ ) (B), deformation potential ( $E_{def}$ ) (C) for each valence, and the elastic constant ( $C_l$ ) (D) are given. The empty circles are the values used in the TB model for  $x = 0$ , 0.2, 0.33, 0.5, 0.6, 0.67, 0.77, 0.8, 0.85, 0.9, and 1. The solid lines are guide to the eye.

#### S4. Single Parabolic Band (SPB) model and Two-Band (TB) model of $(\text{Bi}_{1-x}\text{Sb}_x)_2\text{Te}_3$ for $0 \leq x \leq 1$

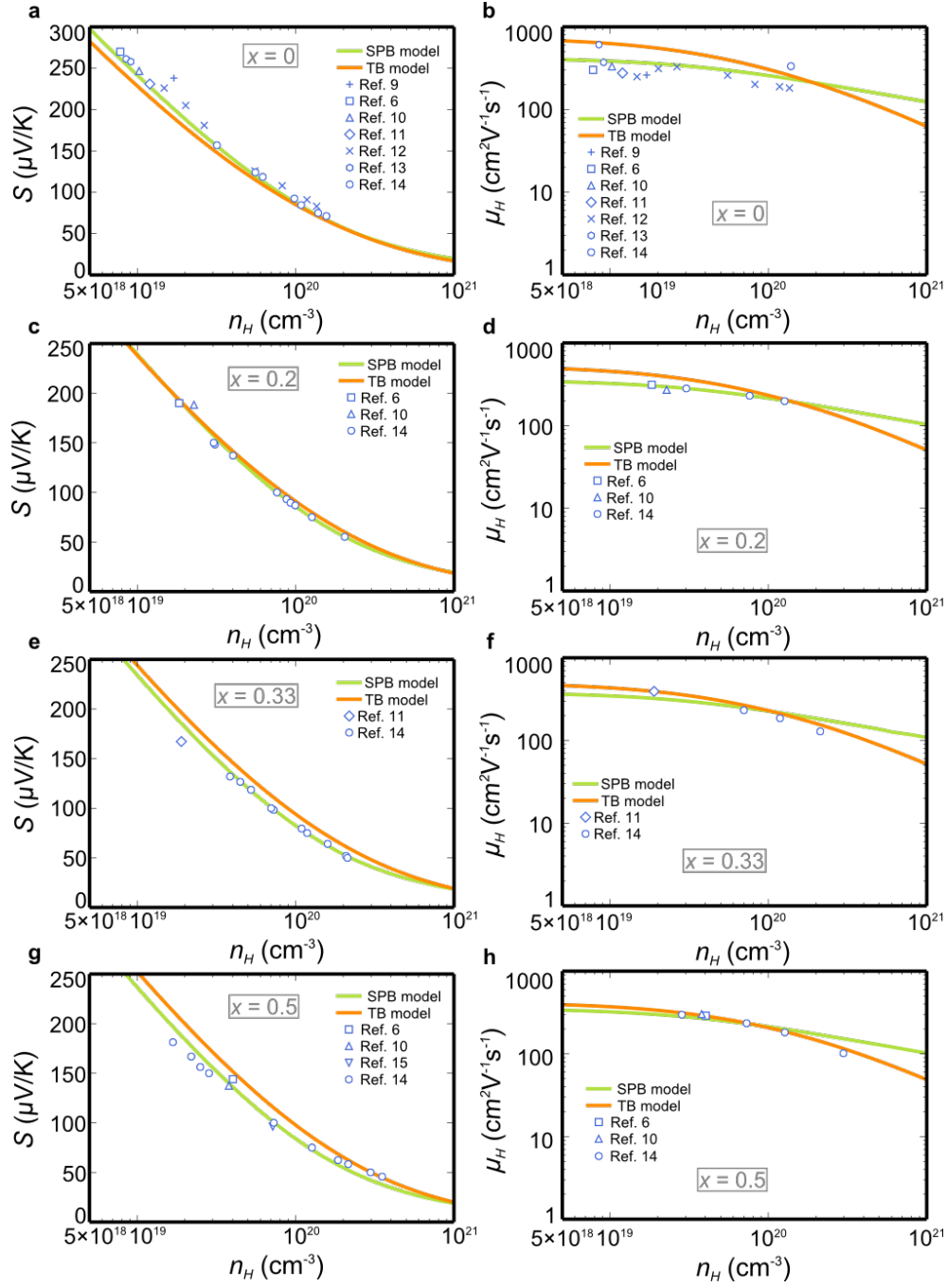


Fig. S4. Transport properties as a function of Hall carrier concentration ( $n_H$ ) for  $(\text{Bi}_{1-x}\text{Sb}_x)_2\text{Te}_3$  at 300 K. The Seebeck coefficient ( $S$ ) and Hall mobility ( $\mu_H$ ) calculated by the TB model for  $x = 0$  (A, B), 0.2 (C, D), 0.33 (E, F), and  $x = 0.5$  (G, H) are shown in orange lines. The TB model was fitted to the literature data from Ref. [6, 9-13], and Ref. [14] (empty shapes in blue). The result of SPB model (green line) was also plotted for comparison.

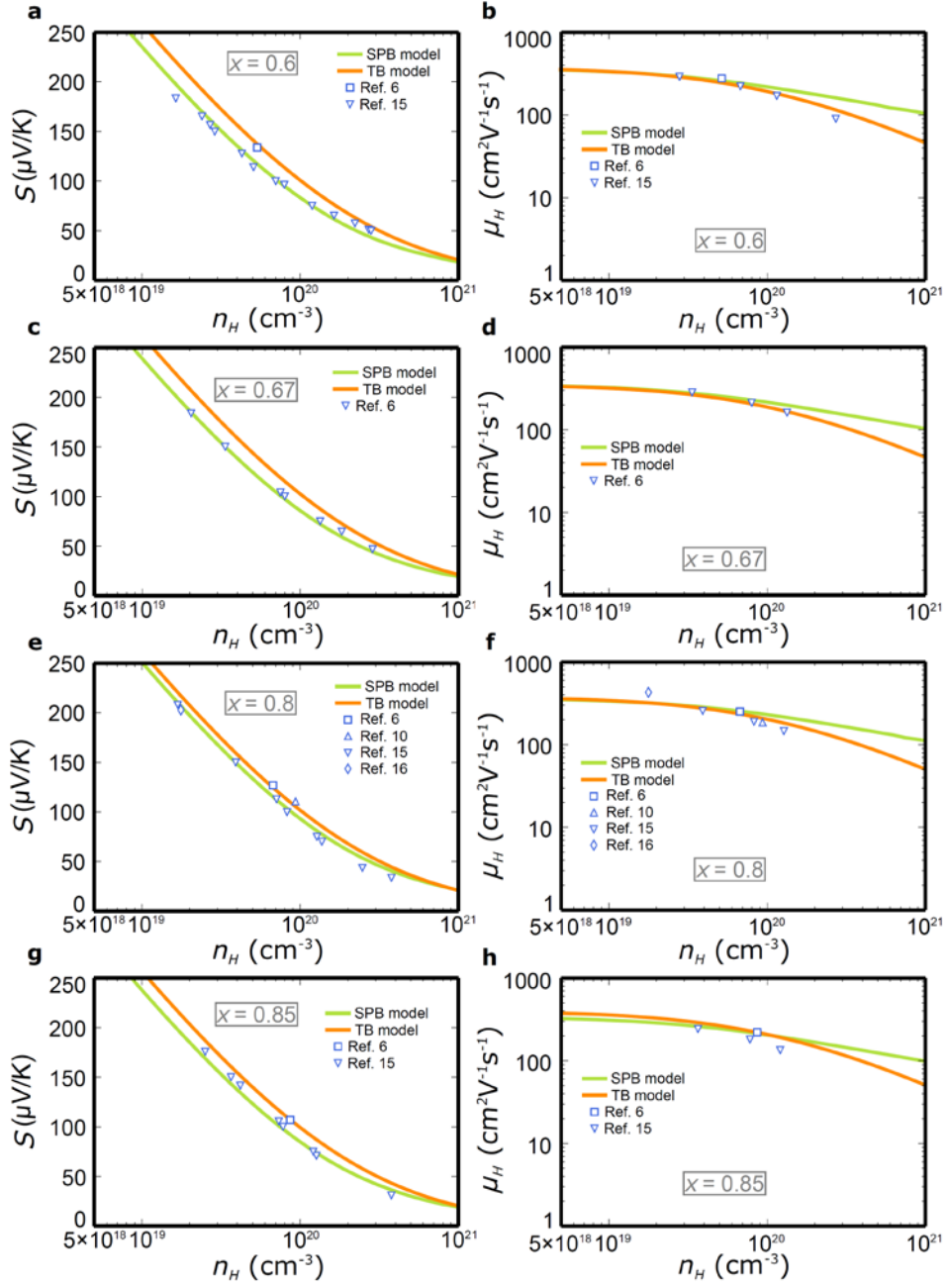


Fig. S5. Transport properties as a function of Hall carrier concentration ( $n_H$ ) for  $(\text{Bi}_{1-x}\text{Sb}_x)_2\text{Te}_3$  at 300 K. The Seebeck coefficient ( $S$ ) and Hall mobility ( $\mu_H$ ) calculated by the TB model for  $x = 0.6$  (A, B),  $0.67$  (C, D),  $0.8$  (E, F), and  $x = 0.85$  (G, H) are shown in orange lines. The TB model was fitted to the literature data from Ref. [6, 10, 15], and Ref. [16] (empty shapes in blue). The result of SPB model (green line) was also plotted for comparison.

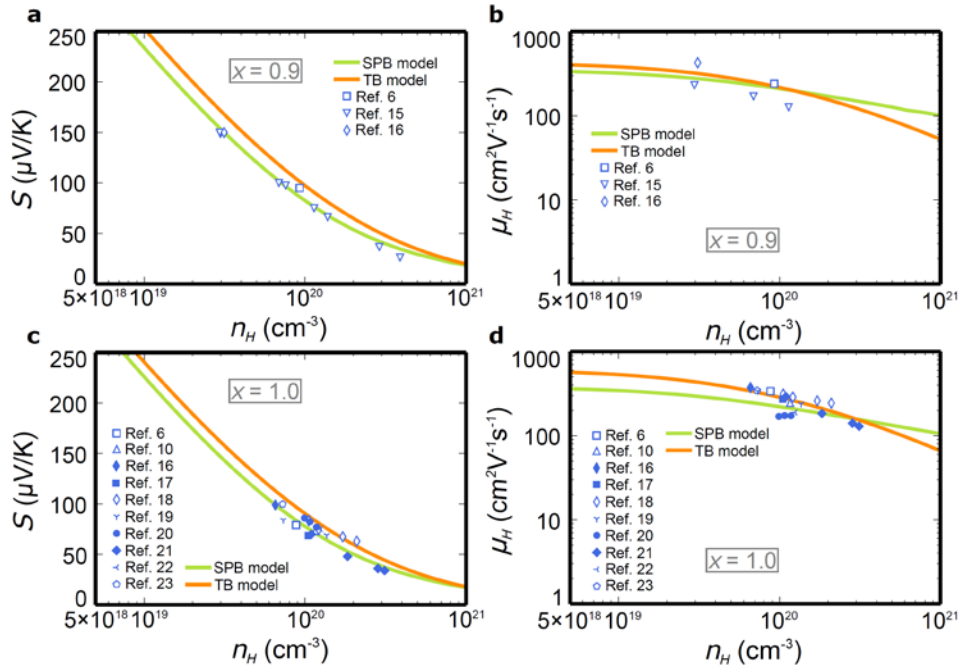


Fig. S6. Transport properties as a function of Hall carrier concentration ( $n_H$ ) for  $(\text{Bi}_{1-x}\text{Sb}_x)_2\text{Te}_3$  at 300 K. The Seebeck coefficient ( $S$ ) and Hall mobility ( $\mu_H$ ) calculated by the TB model for  $x = 0.9$  (A, B) and 1.0 (C, D) are shown in orange lines. The TB model was fitted to the literature data from Ref. [6, 10, 15–22], and Ref. [23] (empty shapes in blue). The result of SPB model (green line) was also plotted for comparison.

## S5. References

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